

Stochastic Model Predictive Control for Gust Alleviation during Aircraft Carrier Landing

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Outline

Motivation

Stochastic
MPC
formulation

Aircraft and
gust modeling

Numerical
Results

Conclusions

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- Motivation
- Stochastic MPC Formulation
- Aircraft and Gust Modeling
- Numerical Results
- Conclusions and Future Work

Motivation

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- Aircraft carrier landing challenges
 - Atmospheric turbulence
 - Carrier airwakes
 - Carrier motion
- Requirement: Real-time optimal feedback control
- Previous research: l_1 adaptive control ([Ramesh and Subbarao, 2016](#)), nominal MPC ([Ngo and Sultan, 2015](#)), dynamic inversion ([Denison, 2007](#))
- Stochastic nature of gusts and airwakes → stochastic optimal control

Stochastic MPC

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- Optimization based control for offset recovery due to gust

$$\begin{aligned} \text{minimize} \quad & \mathbb{E}\left[\sum_{k=0}^{N-1} (x_k^T Q x_k + u_k^T R u_k) + x_N^T Q_N x_N\right] \\ \text{subject to} \quad & x_{k+1} = \bar{A}_d x_k + \bar{B}_d u_k + \bar{E}_d \eta_k \\ & x_k \in \mathbb{X} \\ & u_k \in \mathbb{U} \end{aligned}$$

- Hard polytopic state and control constraints relaxed to individual chance constraints

Stochastic MPC

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- In compact form

$$\mathbf{x} = \mathbf{A}\mathbf{x}_0 + \mathbf{B}\mathbf{u} + \mathbf{E}\boldsymbol{\eta}$$

- Optimal control problem with probabilistic constraints

$$\text{minimize} \quad \mathbb{E}[\mathbf{x}^T \mathbf{Q} \mathbf{x} + \mathbf{u}^T \mathbf{R} \mathbf{u}]$$

$$\text{subject to} \quad \mathbb{P}[\mathbf{x} \in \bar{\mathbf{X}}] \geq 1 - \alpha$$

$$\mathbb{P}[\mathbf{u} \in \bar{\mathbf{U}}] \geq 1 - \beta$$

- Adjust α, β for trade-off between conservatism and performance.
- Intractable with non-convex probabilistic constraints

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- Assume full state feedback, reconstruct past noise from state and control input
- Affine disturbance feedback policy

$$u_k = \sum_{i=0}^{k-1} G_{k,i} \eta_k + s_k$$

- Compact form

$$\mathbf{u} = \mathbf{G}\boldsymbol{\eta} + \mathbf{s}$$

- Suboptimal but tractable; Origin is ISS w.r.t disturbance input under mild assumptions ([Goulart & Kerrigan, 2008](#))

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- Infinite dimensional problem \rightarrow Finite dimensional
- $\eta \sim \mathcal{N}(0, \Sigma)$, individual chance constraints \rightarrow second order cone constraints

$$\Phi^{-1}(1 - \alpha_i) \left\| \bar{H}_{x_i} \mathbf{G} + \mathbf{E} \right\|_2 \leq p_i - \bar{H}_{x_i} (\mathbf{A}X_0 + \mathbf{B}\mathbf{s})$$

$$\Phi^{-1}(1 - \beta_j) \left\| \bar{H}_{u_j} \mathbf{G} \right\|_2 \leq l_j - \bar{H}_{u_j} \mathbf{s}$$

- Constraint set
 - $\mathbb{X} = \{ \mathbf{H}_x \mathbf{x} \leq \mathbf{p} \}$ with $\mathbf{H}_x = \text{diag}(H_x, \dots, H_x)$
 - $\mathbb{U} = \{ \mathbf{H}_u \mathbf{u} \leq \mathbf{l} \}$ with $\mathbf{H}_u = \text{diag}(H_u, \dots, H_u)$
 - $\mathbf{l} = [l^T, \dots, l^T]^T$, $\mathbf{p} = [p^T, \dots, p^T]^T$

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Second order cone program formulation of SMPC

$$\begin{aligned} & \text{minimize} && b^T \mathbf{s} + \text{tr}(\mathbf{M}_2 \mathbf{G} \boldsymbol{\Sigma} + \mathbf{G}^T \mathbf{M}_1 \mathbf{G} \boldsymbol{\Sigma}) + \mathbf{s}^T \mathbf{M}_1 \mathbf{s} \\ & \text{subject to} && \Phi^{-1}(1 - \alpha_i) \|\bar{\mathbf{H}}_{x_i} \mathbf{G} + \mathbf{E}\|_2 \leq k_1 \\ & && \Phi^{-1}(1 - \beta_j) \|\bar{\mathbf{H}}_{u_j} \mathbf{G}\|_2 \leq k_2 \end{aligned}$$

■ where

- $k_1 = p_i - \bar{\mathbf{H}}_{x_i} (\mathbf{A} \mathbf{X}_0 + \mathbf{B} \mathbf{s})$
- $k_2 = l_j - \bar{\mathbf{H}}_{u_j} \mathbf{s}$
- $b^T = 2(\mathbf{A} \mathbf{x}_0)^T \mathbf{Q} \mathbf{B}$, $\mathbf{M}_1 = \mathbf{B}^T \mathbf{Q} \mathbf{B} + \mathbf{R}$ and $\mathbf{M}_2 = 2\mathbf{E}^T \mathbf{Q} \mathbf{B}$

Aircraft motion

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■ Linear longitudinal dynamics with gust

$$\begin{bmatrix} \Delta \dot{u} \\ \Delta \dot{w} \\ \Delta \dot{q} \\ \Delta \dot{\theta} \end{bmatrix} = \begin{bmatrix} X_u & X_w & -u_0 \sin \theta_0 & -g \cos \theta_0 \\ Z_u & Z_w & u_0 \cos \theta_0 & -g \sin \theta_0 \\ M_u & M_w & M_q & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} \Delta u \\ \Delta w \\ \Delta q \\ \Delta \theta \end{bmatrix} \\ + \begin{bmatrix} X_\delta & X_{\delta T} \\ Z_d & Z_{\delta T} \\ M_\delta & M_{\delta T} \\ 0 & 0 \end{bmatrix} \begin{bmatrix} \Delta \delta_e \\ \Delta \delta_T \end{bmatrix} + \begin{bmatrix} -X_u & -X_w & 0 \\ -Z_u & -Z_w & 0 \\ -M_u & -M_w & -M_q \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} u_g \\ w_g \\ q_g \end{bmatrix}$$

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- Aerodynamic coefficients based on the F/A-18 High angle of attack (HARV) model.
- Landing configuration with nominal speed 134 knots and sea level altitude
- Aerodynamic model
 - Leading and trailing edge flaps completely down to 17.6 degrees and 45 degrees
 - Both left and right ailerons down to 42 deg
 - Longitudinal aerodynamics actuator dependency only on elevator deflection

Aircraft motion

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- Assuming steady-state descent flight
 - $u_{trim} = 223.1$ ft/s
 - $w_{trim} = 28.4$ ft/s
 - $q_{trim} = 0$ deg/s
 - $\theta_{trim} = 3.72$ deg
- Corresponds to a trim AOA of 7.26 deg and -3.5 deg glideslope
- Trimmed controls
 - $\delta_e = 11.36$ deg
 - $\delta_T = 0.29$

Gust modeling

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- Only continuous gusts studied
- Spatially varying stochastic processes with Gaussian distribution
- Dryden form given as

$$\Phi_{u_g}(\Omega) = \sigma_u^2 \frac{L_u}{\pi} \frac{1}{1 + (L_u \Omega)^2}$$

$$\Phi_{w_g}(\Omega) = \sigma_w^2 \frac{L_w}{\pi} \frac{1 + 3(L_w \Omega)^2}{(1 + (L_w \Omega)^2)^2}$$

$$\Phi_{q_g}(\Omega) = \frac{\Omega^2}{1 + \left(\frac{4b\Omega}{\pi}\right)^2} \Phi_{w_g}(\Omega)$$

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- For low altitude (~ 200 ft)

$$L_w = 100 \text{ ft} \quad L_u = \frac{h}{(0.177 + 0.000823h)^{1.2}} \text{ ft}$$

$$\sigma_w = 0.1W_{20} \text{ ft/s} \quad \sigma_u = \frac{\sigma_w}{(0.177 + 0.000823h)^{0.4}} \text{ ft/s}$$

- Spectral factorization \rightarrow transfer function \rightarrow linear filter driven by white noise

$$\dot{\xi}_w = A_w \xi_w + E_w \eta$$

$$d = C_w \xi_w$$

Gust modeling

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- Significance of rotary gust q_g if $\sqrt{\frac{\pi b}{16L_w}} C_{m_q} > C_{m_\alpha}$
- Augmenting linearized aircraft model with wind dynamics

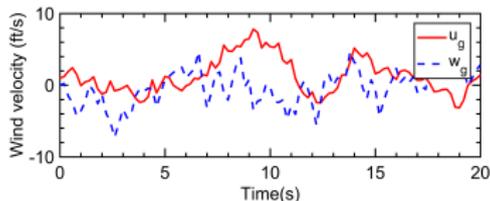
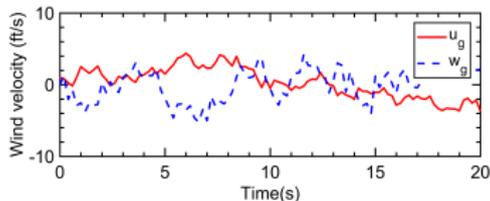
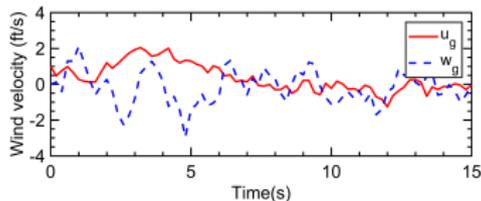
$$\dot{x} = \begin{bmatrix} \dot{x}_l \\ \dot{\xi}_w \end{bmatrix} = \bar{A}x + \bar{B}u + \bar{E}\eta$$

- Discretized version

$$x_{k+1} = \bar{A}_d x_k + \bar{B}_d u_k + \bar{E}_d \eta_k, \quad k \in \mathbb{N}_0$$

Gust modeling

- Wind gust at low, moderate, and high turbulence

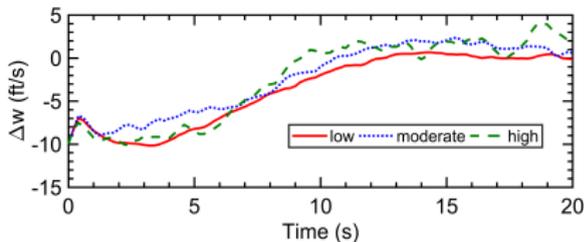
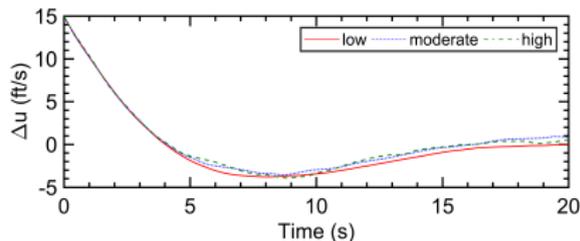


Simulation results

- Perturbed flight with initial state

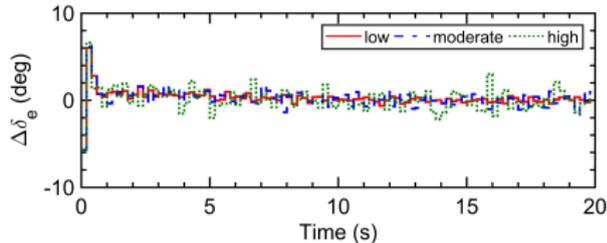
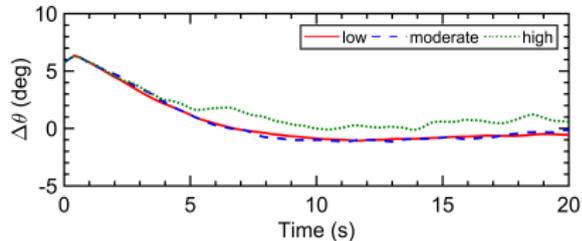
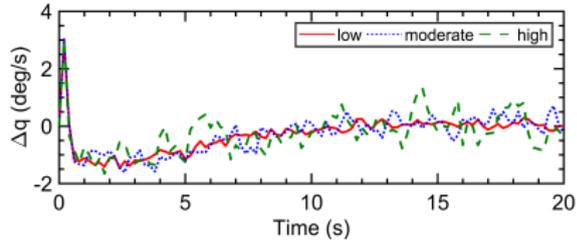
$$x = [15 \quad -10 \quad 0 \quad 0.1]^T.$$

- Prediction horizon $N_p = 10$ s, Total time 20 s.



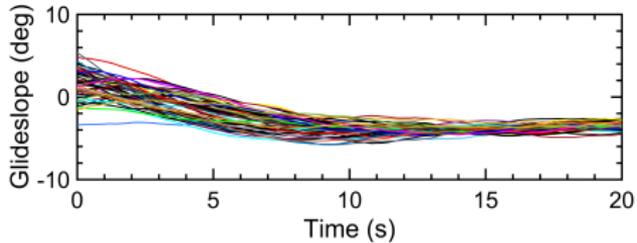
Simulation results

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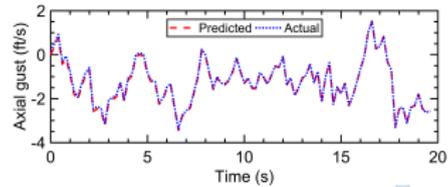
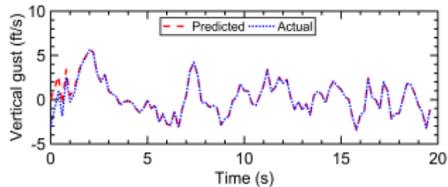


Simulation Results

■ Randomized initial conditions



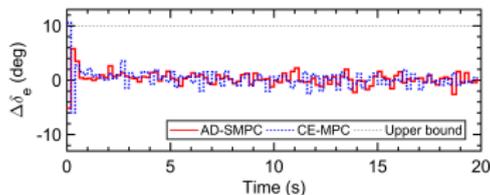
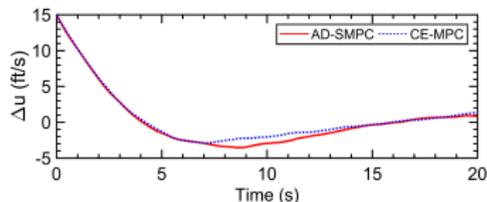
■ Noise/wind reconstruction



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Numerical Results

■ Comparison with certainty equivalent MPC



■ Cost comparison

Method	Cost
AD-SMPC	3.23×10^6
CE-MPC	3.47×10^6

Conclusions and Future Work

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Summary

- Stochastic MPC for aircraft glideslope recovery in gust
- Chance constrained affine-disturbance feedback MPC formulation
- Tractable, cost efficient solution compared to certainty equivalent MPC

Future directions

- Incomplete state information and measurement noise
- Inclusion of carrier burble components